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## Use of spreadsheets in the kinetic analysis of two consecutive first-order reactions

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### Abstract

The present author developed an expression in a previous report that could be applied to the determination of the two rate constants,  $k_1$  and  $k_2$ , for two consecutive irreversible first-order reactions (2CIFR). This expression was solved utilizing various computer methods and rate data (which could be obtained from conversion ( $\alpha$ ) versus time ( $t$ ) curves). Thus, BASICA (IBM), Lotus spreadsheets, and the Paradox data base were employed.

The usual expressions developed for 2CIFR can be converted into dimensionless parameters and variables (DPV). One investigator (to be mentioned subsequently) developed a procedure whereby these DPV could be used to solve for  $k_1$  and  $k_2$  in 2CIFR. His method was rather tedious in that it involved plotting, superposing, and displacement measurements.

In the present paper, a Lotus spreadsheet will be utilized to analyze 2CIFR for  $k$ -values. By means of this analysis, which utilizes dimensionless variables, these  $k$ -values will be obtainable in a matter of seconds once the experimental data is provided.

*Keywords:* Consecutive irreversible first-order reactions; Rate constant; Spreadsheet

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### 1. Introduction

A mathematical expression was recently devised by the author for the concurrent evaluation of two rate constants,  $k_1$  and  $k_2$ , for two consecutive irreversible first-order reactions (2CIFR) [1]. This expression was solved by the use of various computer procedures and rate data (which can be obtained from  $\alpha$ - $t$  curves). Thus, BASICA (IBM) was employed [1] as well as the spreadsheet, Lotus 1-2-3, release 2.2 [2], and the data base Paradox, versions 3 and 3.5 [3, 4].

The usual expressions developed for 2CIFR can be converted into dimensionless parameters and variables (DPV) [5]. Swain [6] devised a procedure whereby these DPV could be utilized to solve for  $k_1$  and  $k_2$  in 2CIFR. His rather tedious method involved the use of graphs, superposition, and the subsequent measurements of displacements.

In the present paper, a spreadsheet, Lotus 1-2-3, release 2.2 (DOS) and 4 (Windows) will be employed to analyze 2CIFR for values of  $k_1$  and  $k_2$ . By means of this analysis, the  $k$ -values will be obtainable in a matter of seconds once the experimental data is provided.

## 2. Theoretical aspects

The 2CIFR may be represented as in the following



In Eqs. (1A) and (1B), A, B, and C denote the starting material, the intermediate product, and the final product, respectively. The use of isothermal TG should enable the estimation of the extent of the reaction depicted in Eqs. (1) on the basis of the amount of gas liberated.

In order to calculate  $k_1$  and  $k_2$  in 2CIFR, reaction times were utilized at three conversions, i.e., 15, 35, and 70% (denoted as  $t_{15}$ ,  $t_{35}$ , and  $t_{70}$ , respectively). In this

Table 1  
Theoretical vs. calculated  $k$ -values at various kappa values using one time ratio (cf. Table 3)

Kappa	Theoretical $k$ -values and corresponding $t$ -values				Calculated $k$ -values	
	$k_1$	$k_2$	$t_{15}$	$t_{70}$	$k_1$	$k_2$
0.100	0.0150	0.0015	23.270	413.000	0.0150	0.0015
0.333	0.0360	0.0120	9.280	80.300	0.0360	0.0118
0.400	0.1000	0.0400	3.300	26.500	0.1000	0.0380
0.500	0.0120	0.0060	27.100	200.700	0.0120	0.0056
0.600	0.2500	0.1500	1.280	8.948	0.2530	0.1380
0.700	0.0028	0.0020	112.700	753.000	0.0028	0.0019
0.800	0.0500	0.0400	6.232	40.060	0.0510	0.0390
0.900	0.0450	0.0405	6.840	42.860	0.0451	0.0404
0.999	0.0500	0.0499	6.081	37.240	0.0499	0.0508
2.000	0.1500	0.3000	1.844	10.230	0.1490	0.3077
3.000	0.2500	0.7500	1.036	5.650	0.2590	0.6210
4.000	0.0750	0.3000	3.280	18.080	0.0831	0.1813

respect, the following expression [1] was used for various fixed values of  $k_1$  and  $k_2$ .

$$2(1 - \alpha) = K_1 \exp(-k_1 t) + K_2 \exp(-k_2 t) \quad (2)$$

where  $K_1 = (k_1 - 2k_2)/(k_1 - k_2)$  and  $K_2 = k_1/(k_1 - k_2)$ . In Tables 1 and 2, various theoretical values of  $t_{15}$ ,  $t_{35}$ , and  $t_{70}$  are given for various  $k_1$  and  $k_2$  values ( $\kappa = k_2/k_1$ ).

A dimensionless expression was also used, i.e.,

$$\delta = 2 - [(1 - 2\kappa)/(1 - \kappa)] \exp(-\tau) - [1/(1 - \kappa)] \exp(-\tau\kappa) \quad (3)$$

where the  $\kappa$  represents kappa,  $\tau = k_1 t$ , and  $50\delta = P\%$  reaction (thus for  $P = 50$ ,  $\delta = 1$ ; for  $P = 100$ ,  $\delta = 2$ , etc.). From Eq. (3), various values of  $\tau$  could be ascertained for  $\kappa$  at  $P$ -values of 15, 35, and 70%. Thus, for example, at  $P = 70$ ,  $\tau$ -values ( $\tau_{70}$ ) could be calculated for various values of  $\kappa$  at  $P = 70$ . Then  $\kappa$  can be obtained as a function of  $\tau_{70}/\tau_{15} (= t_{70}/t_{15})$ . A plot of  $\log(\kappa)$  versus  $\log(t_{70}/t_{15})$  is depicted in Fig. 1. A quartic polynomial was derived correlating  $\log(\kappa)$  and  $\log(t_{70}/t_{15})$  (cf. line B9 of Table 3). In this table, T7015T denotes  $t_{70}/t_{15}$  and K7015K in line B10 of Table 3 now denotes  $\kappa$  for the ratio  $t_{70}/t_{15}$ . Lastly, from the preceding,  $\tau_{15}$  could be correlated with K7015K by means of a polynomial of the 6th degree (cf. line B11 of Table 3). Also, from the preceding,  $k_1 = \tau_{15}/t_{15}$  and  $k_2 = k_1 \times \text{K7015K}$ . Thus, in Table 3,  $k_1 = 0.3427/0.367 = 0.934$  and  $k_2 = k_1 \times 0.1921 = 0.1794$ , as indicated on line A27 of Table 3. In these calculations, values in cells B5, C5, A36, and B36 of Table 3 were utilized. Besides using two reaction times and one ratio ( $t_{70}/t_{15}$ ) to estimate values of  $k_1$  and  $k_2$ , three reaction times and three time ratios were also employed, i.e.,  $t_{70}/t_{15}$ ,  $t_{70}/t_{35}$ , and  $t_{35}/t_{15}$  (cf. Tables 2 and 4). Similar  $k$ -value calculations, as noted in the preceding, were also carried out in Table 4.

Table 2

Theoretical vs. calculated  $k$ -values at various kappa values using three time ratio (cf. Table 4)

Kappa	Theoretical $k$ -values and corresponding $t$ -values					Average calculated $k$ -values	
	$k_1$	$k_2$	$t_{15}$	$t_{35}$	$t_{70}$	$k_1$	$k_2$
0.100	0.0150	0.0015	23.270	71.870	413.000	0.0150	0.0015
0.333	0.0360	0.0120	9.280	25.710	80.300	0.0360	0.0120
0.400	0.1000	0.0400	3.300	8.970	26.500	0.1010	0.0397
0.500	0.0120	0.0060	27.100	71.800	200.700	0.0120	0.0059
0.600	0.2500	0.1500	1.280	3.300	8.948	0.2520	0.1478
0.700	0.0028	0.0020	112.700	287.000	753.000	0.0028	0.0019
0.800	0.0500	0.0400	6.232	15.700	40.060	0.0500	0.0402
0.900	0.0450	0.0405	6.840	17.020	42.860	0.0451	0.0408
0.999	0.0500	0.0499	6.081	15.000	37.240	0.0500	0.0512
2.000	0.1500	0.3000	1.844	4.292	10.230	0.1480	0.3007
3.000	0.2500	0.7500	1.036	2.362	5.650	0.2560	0.6196
4.000	0.0750	0.3000	3.280	7.438	18.080	0.0814	0.1884

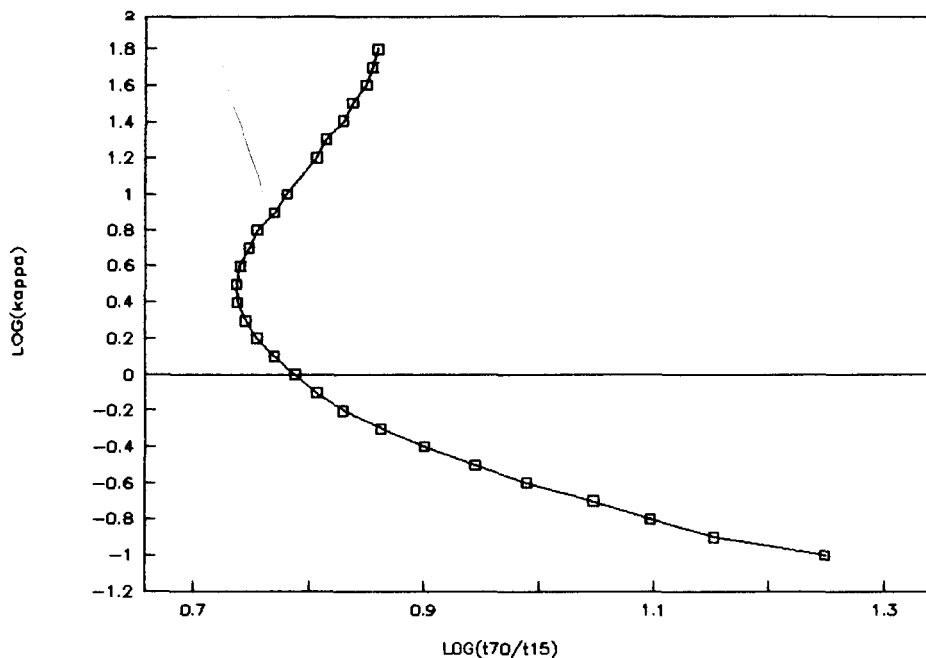


Fig. 1

### 3. Results and discussion

The Lotus worksheet in Table 3 was employed to obtain the calculated values of  $k_1$  and  $k_2$  in Table 1. Similarly, the worksheet in Table 4 was used to obtain the calculated  $k$ -values in Table 2. As an illustration, experimental data [6] for  $t_{15}$  and  $t_{70}$  were entered into cells B5 and C5, respectively (cf. Table 3). Then the run command was given for the macro, lines A8–A12 (alt-W for DOS and ctrl-W for Windows). Within a few seconds, the results for  $k_1$  and  $k_2$  appeared in cells C27 and E27, respectively, i.e., 0.934 and 0.1794 h<sup>-1</sup> (the reaction times were in hours). The average reported results [6] were  $k_1 = 0.937$  h<sup>-1</sup> and  $k_2 = 0.180$  h<sup>-1</sup>, in excellent agreement with the spreadsheet results. Similar average  $k$ -values were obtained in Table 4 using three time ratios. In obtaining his results, Swain also utilized three time ratios, i.e.,  $t_{70}/t_{35}$ ,  $t_{70}/t_{15}$  and  $t_{35}/t_{15}$ , and reported the average of his results. In Table 3, only one ratio, i.e.,  $t_{70}/t_{15}$ , was used since it was observed that this time ratio alone could afford calculated  $k$ -values which were in excellent agreement with corresponding theoretical values. However, this good agreement (cf. Table 1) only held up to a  $\kappa$ -value of 2.0, after which it became increasingly poor as  $\kappa$  was increased to a value of four. This could be accounted for as follows. From Fig. 1, it can be observed that in the plot of  $\log(\kappa)$  versus  $\log(t_{70}/t_{15})$ , at a value of  $\log(\kappa)$  of ca. 0.4 ( $\kappa = 2.5$ ), the curve starts to turn back toward the previous portion of the curve causing double values of  $\log(\kappa)$  for corresponding singular

Table 3

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A      A      B      C      D      E      F      G      H      I      J      K      L      M
1      This pgm. calculates the 2 rate constants, k1 and k2 for 2 consecutive irreversible first-order reactions using 1 time ratio
2
3
4      Time (15%)      Time(70%)
5      0.367          4.2
6      =====
7
8      W( (let T7015T @log(170A150))-
9      (let K7015K 88 8181-342 941*(T7015T+498 0364*(T7015T)^2-322 259*(T7015T)^3+77 84512*(T7015T)^4)-
10     (let K7015k 10*(k7015k))-
11     (let tau15t 0.3551-0.068763*k7015k+ 0.22313*(k7015k)^2-.0049327*(k7015k)^3+ 0.0064561*(k7015k)^4-.000044658*(k7015k)^5+ 0.000012527*(k7015k)^6)-
12     (home)(goto)A23--
13
14
15
16     Range Values
17     K7015K      A36_A36
18     T15T        B5_B5
19     T7015T      C36_C36
20     T70T        C5_C5
21     TAU15T      B36_B36
22     W          B8_B8
23
24
25
26
27     VALUES OF K1 AND K2 ARE, RESP.      0.934      AND      0.1784
28     BASED ON VALUES OF KAPPA(70%/15%) AND OF Tau(15%)
29
30
31
32
33
34
35
36     K7015K      Tau15T      T7015T
37     0.1821      0.3427      1.0588
38
39
40
41
42
43
44
    
```

Table 4

```

A      A      B      C      D      E      F      G      H      I      J      K      L      M
1      Program calculates the two rate constants, k1 and k2, for 2 consecutive irreversible first-order reactions using 3 time ratios
2
3
4      Time (15%)      Time (35%)      Time(70%)
5      0.367          1.067          4.2
6      =====
7
8      W( (let T3515T @log(135A151))-
9      (let K3515K 254 709-2307*(T3515T+7865 95*(T3515T)^2-11889 67*(T3515T)^3+6718 6394*(T3515T)^4)-
10     (let k3515k 10*(k3515k))-
11     (let tau35t 1.114145- 80025*k3515k+ 30866*(k3515k)^2-0.085931*(k3515k)^3+ 0.12794*(k3515k)^4-.0095827*(k3515k)^5+ 0.0002833*(k3515k)^6)-
12     (let T7035T @log(170A355))-
13     (let K7035K 463 184-4966 43*(T7035T+22078 1*(T7035T)^2-52026 14*(T7035T)^3+68448 21*(T7035T)^4-47642 8*(T7035k)^5+ 13701 66*(T7035k)^6)-
14     (let k7035k 10*(k7035k))-
15     (let T7015T @log(170A151))-
16     (let K7015K 88 8181-342 941*(T7015T+498 0364*(T7015T)^2-322 259*(T7015T)^3+77 84512*(T7015T)^4)-
17     (let K7015k 10*(k7015k))-
18     (let tau15t 0.3551-0.068763*k7015k+ 0.22313*(k7015k)^2-.0049327*(k7015k)^3+ 0.0064561*(k7015k)^4-.000044658*(k7015k)^5+ 0.000012527*(k7015k)^6)-
19     (goto)A23--
20
21
22
23
24
25
26
27     THE VALUES OF K1 AND K2 ARE, RESP.      0.943      AND      0.188
28     BASED ON VALUES OF KAPPA(35%/15%) AND OF Tau(35%)
29
30     THE VALUES OF K1 AND K2 ARE, RESP.      0.934      AND      0.173
31     BASED ON VALUES OF KAPPA(70%/35%) AND OF Tau(15%)
32
33     THE VALUES OF K1 AND K2 ARE, RESP.      0.934      AND      0.180
34     BASED ON VALUES OF KAPPA(70%/15%) AND OF Tau(15%)
35
36
37     Avg values      STD      0.9367      0.1802
38     0.004          0.006
39
40
41
42
43     K3515K      T7035T
44     0.1994      0.5951
45     K7035K      T3515T
46     0.1850      0.4625
47     K7015K      T7015T
48     0.1926      1.0586
49     Tau35T      Tau15T
50     1.0061      0.3427
51
52
53
54
55
56
57
58
59
60
    
```

values of  $\log(t_{70}/t_{15})$ . Thus, a polynomial correlation would not be expected to afford calculated  $k$ -values in good agreement with theoretical  $k$ -values when  $\kappa$  exceeded a value of two, as indicated in Table 1. In order to present a more complete picture, average  $k$ -value results are also presented in Table 2 using the three ratios  $t_{70}/t_{35}$ ,  $t_{35}/t_{15}$ , and  $t_{70}/t_{15}$  and expressions given in Table 4. These average  $k$ -value results, also agreed well with the theoretical, and similar limitations apply as previously indicated for the  $t_{70}/t_{15}$  ratio. Finally, it should be mentioned that the ultimate validity of the calculated  $k$ -values should be established by comparing conversion values (experimental or theoretical) with corresponding conversion values calculated by using these  $k$ -values in Eq. (2).

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